

## MANDATORY WOOD FRAME SOFT-STORY RETROFIT PLAN REVIEW LIST-DIVISION 93 (2014 LABC)

			•		
	Plan Check Submittal Date:		Expiration Date:		
	PCIS Application Number:		Plan Check No.:		
	Address				
	Applicant Name:		Phone No.:		
	Plan Check Engineer:	Email:			
	Phone No:		firstname.lastname@lacity.org	3	
<u>fe</u>	Your feedback is important to us. Please visit <a href="http://ladbs.org/our-organization/customer-services/customer-feedback-form">http://ladbs.org/our-organization/customer-services/customer-feedback-form</a> to complete the Customer Survey.				
	STRUCTIONS FOR PROCEEDING WITH THE PLAN				
1.	Review all the items selected as marked on this Plan R calculations.	eview List and t	ne notes marked on the se	t of plans and	
	Address each item and revise the plans and/or structural a written response, addressing each item and referencing package. For any questions related to this plan review, plant review,	ng the location ease e-mail or c	on the revised plans and all the plan check engineer	/or calculation	
3.	Once all corrections have been addressed, please email the A verification appointment will then be scheduled. Verification	•	. ,	•	<u>}</u> _
4.	For the verification appointment, bring the originally check and calculations, the written response, and this Plan Revieresult in appointment postponement or cancellation at	ew List. <mark>Failure</mark> 1	to supply all necessary d		
5.	During the appointment, the plan check engineer will go over been corrected to comply with the code requirements and issued.				е
IM	PORTANT ITEMS TO READ:				
1.	Your early attention is highly recommended for the approv Clearance Summary Worksheet due to possible time delay		other Departments as liste	d in the	
2.	The permit application will expire 18 months from the plan	check submittal	date.		
3.	Please be advised that the permit will be issued upon verif The approval of plans does not permit the violation of any law.	•			
4.	Referenced numbers at the end of each correction are coordinated the current Zoning Code and enacted code amendments to		e 2014 edition of the Los A	ingeles Codes,	
The following documents are available online, <a href="www.ladbs.org">www.ladbs.org</a> , to provide guidance and assistance in compliance to Division 93 of the Los Angeles Municipal Code (LAMC). Review the following checked documents and revise the plans and calculations accordingly.					
	Mandatory Wood Frame Soft-story Retrofit, Structural Design Guidelines P/BC 2014-137	<u> </u>	Observation Report Form		8
	Mandatory Earthquake Hazard Reduction in Existing Wood-Frame Buildings with Soft, Weak or Open-Front Walls Ordinance 183893 / 184081	Resisting	Design Guidelines for St Frames n for Expansive Soils	P/BC 2008-09	
	Standard Quality Assurance Plan for Steel	Summary	of Parking Regulation	P/ZC 2002-01	1
	Moment Frames	☐ Parking Lo	ot Design	P/ZC 2002-00	1

## **PART I: GENERAL REQUIREMENTS** A. PERMIT APPLICATION **B. ADMINISTRATION** 1. Provide a fully dimensioned plot plan to scale, in ink, and 1. Each sheet of the architectural and structural plans must copy onto the attached "Plot Plan Sheet". bear the signature, license number and expiration date of an architect or engineer licensed in the State of California. 2. Project valuation is revised to \$ Pay additional plan check fees of \$ 2. The address of the building is required on all plans. Name / address of the owner is required on first sheet. The name 3. Provide complete and correct legal description (Tract, and address of the consultants are required on their plans. Block, Lot, and Grant Deed). Provide complete information for applicant, owner, engineer, architect, and 3. Two sets of plans will be required during permit issuance. contractor. Plans must be: 106.3.2.2, 106.3.3 a. Quality blue or black line drawings with uniform and 4. The permit application must be signed by the property owner, a licensed contractor, or an authorized agent at light background color. the time the permit is to be issued: b. Min. 11" x 17" size with minimum 1/8" lettering size. a. Tor owner-builder permits: Owner's signature can be c. Sticky back details must produce prints without verified with owner's driver license. Owner's contrasting shades of background color. representatives must present owner's approval with a notarized letter from the owner. 4. The final set of plans must be stamped and approved by (Fire Dept.), ( b. $\square$ For contractor building permits: Prior to the issuance 5. Provide a complete description for the entire scope of of a building permit, the contractor shall have the work on the plans. following: 6. Provide the following with each set of plans: i. Certificate of Worker's Compensation Insurance made out to the Contractors State License Board. ☐ Floor Plans ☐ Four Elevations ☐ Construction Section ☐ Foundation Plans ii. Notarized Letter of Authorization for agents. ☐ Framing Plans ☐ Structural Details iii. Copy of Contractors State License or pocket ID. 7. Remove all plans, details or notes that do not pertain to iv. Copy of City of Los Angeles business tax the project. registration certificate or newly paid receipt for one. 8. Provide a fully dimensioned plot plan to scale showing: Legal Description 5. ☐ CLEARANCES ☐ Property Lines Obtain all the clearances noted on the attached ☐ Building Lines ☐ Area of Work "Clearance Summary Worksheet". To prevent any time ☐ Parking Space ☐Alley / Street Center ☐ Use/Size of all Buildings delay, please go to each listed agency immediately for sign-offs. Each agency's process of approval may take some time. Note that all conditions of approval must be met to obtain the permit and/or final inspection approval. PART II: ZONING CODE REQUIREMENTS (Allow time for discretionary approval process from City Planning if zoning requirements can't be met.) 1. Show on plans that no required parking spaces have been 5. Plans shall be drawn to scale (around 1/8"=1"), showing compromised or removed. Show that the existing backup aisle widths, circulation driveway, stall widths, and stall aisles and turning radius will be maintained and not width increase for obstructions and end stall conditions. affected. 12.21A5(b) 2. Plans show a reduction in parking. Provide ( 6. Clearly show on plan, existing fence wall surrounding the ) paved parking and driveway area. A 5'-9" high wall is required parking spaces per latest Certificate of Occupancy or latest along the interior lot line(s) and 3' max high wall along the permit on record noting the required parking. 12.21A4, 12.21A5 property line(s) fronting a street. A solid concrete or masonry wall of 6" thick construction is required for parking 3. Projection of ( ) into the ( ) yard/passageway is areas with over 4 cars 12.21A6(d),(e),(f) not permitted or limited to ( 12.22C20 ). 7. Comply with **Zoning Information** file # 4. Relocated and/or new parking spaces shall comply with current Zoning Code requirements. Comply with parking design standards. 12.21A.5 (h)

## PART III BUILDING CODE REQUIREMENTS

<ul><li>A. GENERAL PLANS</li><li>1. ☐ Identify and reference all sections and details as to their</li></ul>	including the name(s) of the individuals or firms who will perform the work. The inspection program shall be shown on the first sheet of the structural plans. 1704
location on the plan and elevation views.  2. Justify that the wall line along gridline or ( N , S , E , W ) elevation is/are not weak, soft, or open-front wall line. Provide pier/wall lengths on the elevation for field verification.	3. Include the following (Steel Moment Frame)  Connected components  Removal of backing bars  Placement of reinforcing fillets  Presence of continuity plates
3. Cross reference all calculations for joists, beams, shear walls, etc., to framing/floor plans.	<ul><li>☐ Welding of continuity plates</li><li>☐ Presence and type of doubler plates</li><li>☐ Welding of doubling plates</li></ul>
4. Submit structural calculations / design details for	<ul><li>☐ Configuration and finish of access holes</li><li>☐ Placement of beam stiffeners</li></ul>
5. Provide calculations and detailing for complete load path.	<ul> <li>Contour and finish of RBS profile</li> <li>Placement of weld for web connection</li> <li>Type and placement of bolts</li> <li>Inaccessible conditions</li> </ul>
6. Shoring shall be provided during construction per housing approval.	4.  Where special inspection or testing is required, the registered design professional in "responsible charge"
7. A floor plan of the building is required to show the location of proposed retrofit. The floor plan must also show exiting scheme from the building in which moment frames will be	shall include a "Statement of Special Inspections" on the plans.
placed.  8. ☐ Structural plans, details, and calculations are required for the construction of moment frames.	5. The following structural products shall comply with an approved Los Angeles City Research Report. Copy the conditions of approval onto the plans and show
<ol> <li>The plans and/or structural analysis are incomplete. A resubmittal is required and additional fees will apply.</li> </ol>	compliance with those conditions.  Hold-downs Prefab Shear Wall Panels Epoxy Anchors Expansion Anchor Bolts
10. The engineer or architect shall provide the following statement on the approved plans:  "I am responsible for designing this building's seismic strengthening in compliance with the minimum regulations of the Mandatory Earthquake Hazard Reduction. In Existing Wood-Frame Buildings with Soft, Weak, or Open-Front Walls (LAMC Division 93)."	☐ Straps ☐ Moment Frame ☐ Others such as  6.☐ Add the following notes onto plans:  a. ☐ Contractors responsible for the construction of a seismic force resisting system/component listed in the "Statement of Special Inspection" shall submit a written statement of responsibility to the LADBS
<ul><li>B. MATERIAL SPECIFICATION &amp; INSPECTIONS</li><li>1. Specify the following items on plans:</li></ul>	Inspectors and the owner prior to the commencement of work on such system or component. 1709.1 1
a. Type of soil and bearing value per	b. Pre-Construction Meeting: The owner or owner's
b. Standard 2,500 psi concrete	representative shall arrange a preconstruction meeting to be attended by the engineer or architect
c. 3000 psi min. for grade beams and piles/piers.	responsible for the structural design, Structural
<ul> <li>d. ☐ Type and f'<sub>m</sub> of masonry units. Proportions of mortar and grout mixes.</li> </ul>	Observer, contractor, affected subcontractors, deputy inspectors, and the building inspector.
e.  Type of Structural Steel, Structural Pipe, Tubing, Reinforcing bars.	<ul> <li>c.   Continuous Special Inspection by a registered deputy inspector is required for:</li> <li>Field welding</li> </ul>
<ul> <li>f.          Grade, species, and moisture content of all lumber.     </li> <li>Type and grade of plywood sheeting.</li> </ul>	<ul><li>☐ Special moment resisting concrete frame</li><li>☐ High load wood diaphragms</li></ul>
2. Structural Observation is required for this project. The engineer of record shall prepare an inspection program,	<ul><li>☐ Driven deep foundation</li><li>☐ Cast-in place deep foundations</li></ul>

☐ Concrete strength f' <sub>c</sub> >2,500 psi	f. Basic seismic-force-resisting system(s).
☐ High strength bolting	g.   Design base shear. Total weight of building.
Sprayed-on fireproofing	_
☐ High-lift grouting	h. $\square$ Seismic response coefficient(s), $C_s$ .
	i. Response modification factor(s), R.
d. Periodic Special Inspection by a registered deputy	j.   Analysis procedure used.
inspector is required for  ☐ Wood shear wall	k.  Redundancy factor used.
☐ Special moment resisting concrete frame	_
☐ High load wood diaphragms	I.   The design load bearing value of soils
☐ Shear panels	2. Seismic Design Category (SDC) shall be based on LABC
☐ Cast-in place deep foundations	Table 1613.3.5(1) and Table 1613.3.5(2). When $S_1$ , is
☐ Concrete strength f' <sub>c</sub> >2,500 psi	greater than or equal to 0.75, the building shall be
☐ High strength bolting	assigned to SDC E for Risk Category I, II, or III and
☐ Sprayed-on fireproofing	assigned to SDC F for Risk Category IV.
☐ High-lift grouting	3. Design Base Shear
<b>1705</b>	
e.  Foundation sills shall be naturally durable or	<ul><li>a.  The design base shear shall be 75 percent of the value 12.8-1 of ASCE 7.</li><li>9309.2</li></ul>
preservative-treated wood. 2304.11.2.4	b.   The upper system has a lower response
f. $\square$ Field welding to be done by welders certified by	modification coefficient, the design coefficients (R,
LADBS for	<sub>0</sub> , C <sub>d</sub> ) of the upper system shall be used for the
Structural Steel	strengthening system. ASCE 7 sec 12.2.3.1
Reinforcing Steel	Note: However, R need not be less than 3.5
Light Gauge Steel	provided the strengthened structure will not have any
g.   Shop welds must be performed in a LADBS	vertical structural irregularities as defined in ASCE 7.
licensed fabricator's shop.	The deflection amplification factor C <sub>d</sub> value shall be 3
h.   LADBS licensed fabricator is required for	and overstrength factor, $\Omega_{0}$ , shall be 3 which are consistent with the R value of 3.5 as specified in the
Structural Steel	seismic provisions of ASCE 7 for the lateral resisting
Glu-lam(grade/species) 2012 NDS Sup T'5-A	system. Cantilever Column Systems shall still use the
<u> </u>	corresponding values.
i.  Provide lead hole 40% - 70% of threaded shank	c.  Where a combination of different structural systems
diameter and full diameter for smooth shank portion.	is utilized to resist lateral forces in the same direction,
j.   Special inspection by a deputy inspector is required	the value of R used for design in that direction shall
for shear panels where the fastener spacing of the	not be greater than the least value of R for any of the
sheathing is 4 inches on center or less.	systems utilized in that direction.
<u> </u>	ASCE 7 sec 12.2.3.3
<ul> <li>k.    ☐ A copy of the Los Angeles Research Report and/or conditions of listing shall be made available at the job</li> </ul>	4. ☐ Seismic Mass
site.	a.  Consider 10psf partition load per floor area.
	ASCE 7 sec 12.7.2
C. <u>LATERAL LOADS</u>	b Capaidar 15 per roof and floor dood load or provide
1. Earthquake design data - The following information	<ul> <li>b.          Consider 15 psf roof and floor dead load or provide detailed roof and floor dead load calculation.</li> </ul>
related to seismic loads shall be shown on the plan.	<u>_</u>
1603.1.5, 1603.1.6	c.  Include roof and floor dead load, psf, on drawings
a.  Seismic importance factor I, and risk category.	and next to framing plan on each level.
b. $\square$ Mapped spectral response accelerations, $S_s$ and $S_1$ .	d.  Consider ceiling framing and finishing weight for
c. Site class.	sloped roofs.
d. $\square$ Spectral response coefficients, SD <sub>s</sub> and SD <sub>1</sub> .	e. Add 15 psf to floor dead load for concrete topping.
e.  Seismic design category.	f. Add note under the floor and roof dead load on plans that there is no concrete topping assumed in dead load calculations. Contractor to verify in field.

or provide detailed exterior wall dead load calculations.	shall be interconnected and capable of resisting the seismic force required. Provide calculations and details to show that collector elements, splices, and connections to	
<ul> <li>h. Consider 5 psf for existing or possible future installation of solar panels on the roof.</li> </ul>	resisting elements have the strength to resist the combined loads resulting from the load combinations with	
<ul> <li>i. Consider exterior walls both in direction and perpendicular to the direction of soft wall line in seismic mass.</li> </ul>	overstrength factor per ASCE 7-10 Sec.12.10.2.1 and Sec.12.14.7.3.	
<ul> <li>j.    Consider 8 psf for existing or new stucco cover under the existing ceiling above parking area.</li> </ul>	<ol> <li>Lumber and structural wood panel diaphragms shall not be considered as transmitting lateral forces by rotation.</li> <li>SDPWS sec 4.2.5</li> </ol>	
5. Strengthening system with concrete walls or masonry walls or steel braced frames shall not be permitted . 9309.3	E. ALTERNATIVE DESIGN METHODS  Pursuant to section 104.2.6, LADBS has approved the following alternative design methodologies whose objective is to improve the whole first story seismic performance.  9309.5	
6. Horizontal Structural Irregularities in buildings with 3 or more stories shall meet the additional requirements of		
ASCE 7 12.3.2.1, referenced in Table 12.3-1 "Horizontal Structural Irregularities" 9309.4	<ol> <li>Appendix Chapter A4, 2012 International Existing Building Code with the following conditions:</li> </ol>	
7. Vertical Distribution of Seismic Forces over the height of	a.  Comply with all standards as prescribed.	
the structure shall be based on ASCE 7-10 Section 12.8.3.  8. Anchorage Requirements for Buildings on Hillsides. Any	<ol> <li>ASCE 41-13, Seismic Evaluation and Retrofit of Existing Buildings with the following conditions</li> </ol>	
portion of a building constructed on or into a slope steeper than one unit vertical in three units horizontal (33% slope), must comply with the provisions of LAMC Division 94.	<ul> <li>a. Design to meet the Rehabilitation Objective (Section 1.4) (Life Safety Performance Level: S-3) for the BSE-1 earthquake hazard level.</li> </ul>	
9. Story Drift Limitations	<ul> <li>D. Retrofit strength need not exceed 1.3 times the strength of story above.</li> </ul>	
<ul> <li>a.  The calculated story drift for each retrofitted story shall not exceed the allowable deformation compatible with all vertical load-resisting elements and 0.025 time the story height</li> </ul>	3. FEMA P-807, Seismic Evaluation and Retrofit of Multi-Unit Wood-Frame Buildings with Weak First Stories with the following conditions.	
b.  Calculate seismic drift based on deflections of each	a.   The entire story must be analyzed and designed.	
level with $C_d$ and I factors using strength level forces in accordance with ASCE 7-10 Sec.12.8.6.	b. The spectral demand shall be 0.5S <sub>MS</sub> , calculated in accordance with ASCE 7-10 section 11.4 except that	
c.  Verify that the stiffness of the strengthened system is greater than 70% of the Stiffness of the floor above	for sites in site class E, the value of Fa shall be taken as 1.3.	
or limit the drift ratio to 2.0%.	<ul> <li>c.           Acceptable performance level shall be based on         drifts corresponding to Onset of Strength Loss in the         seismic force-resisting wood-frame elements.</li> </ul>	
<ul><li>D. <u>HORIZONTAL DIAPHRAGM</u></li><li>1. ☐ Diaphragm cantilever is greater than 25% of diaphragm</li></ul>	d. The maximum limit probability of exceedance (POE)	
depth. Provide calculations to show diaphragm adequacy and shear transfer to the seismic resisting element.	for evaluation/retrofit design shall be 20%.	
2. Diaphragm aspect ratio shall not exceed 3:1.	e. Limit diaphragm ratio to 2:1.	
3. Provide calculations and details on the plans for the sub-diaphragm and continuous cross-tie system required for all wood diaphragms providing lateral support to existing masonry or concrete walls. The spacing of continuous ties shall not exceed 40 ft. per LABC 1613.5.4.		

G. WOOD SHEAR WALLS	11. Per structural calculations, show size, location and
1. Provide a shear wall schedule on the plans and specify the maximum design shear load for each shear wall type.	embedment length of all anchor bolts (including HD bolt anchors) on foundation plan.
Limit the design shear wall loads to those allowed by Code. Clearly indicate on the plans all plywood and drywall shear walls.	12. The anchor or group of anchors shall be designed for the maximum tension that can be transmitted to the anchor or group of anchors based on the development of a ductile
2. The is inadequate to resist lateral/ uplift forces. Show roof/floor diaphragm nailing, wall bracing, shear connections, tie downs and hold-down anchors. Submit lateral design.	yield mechanism in the attachment in flexure, shear, or bearing, or a combination of those conditions, and considering both material over strength and strain hardening effects for the attachment. The anchor design tensile strength shall be calculated from D3.3.4.4.
3. Provide shear connection details, properly referenced, at the top and bottom of all shear walls.	ACI 318 Appendix D,D.3.3.4.3
4. The horizontal distribution of seismic shear to wood structural panel shear walls shall be in accordance to ASCE 7-10 Section 12.3.1.1.	13. Provisions under Section 1908 and Table 1908.2 do not apply to anchors installed in hardened concrete subject to earthquake loads. Justify the capacity of tie down bolt in concrete footing/wall/deck per ACI 318-11 Appendix D with
5. Provide LARR number for screws used in steel sheets or cold-formed steel framed walls sheathed with wood structural panels. Shear values for steel sheets or cold-formed steel framed walls sheathed with wood structural panels shall conform to the requirements in AISI-Lateral C2.2.1 and C2.2, respectively. Allowable values shall be in	factored design loads.  1908.1  14. When bolting to an existing footing, provide a copy of the LA Research Report approval for the type of bolt, allowable design loads and required edge distances. Deputy inspection is generally required.
conformance with T'C2.1-3, taking in to account the corresponding reductions per C2.1 (AISI-Lateral).	15. Provide LARR number for hold-down connectors. The capacity of hold-down connectors that do not consider cyclic loading of the product shall be reduced to 75% of the
6. Wood structural panel shear walls shall meet the story drift limitation of ASCE 7-10 Section 12.12.1 Conformance shall be determined by testing or calculations. Calculated deflection shall be determined according to equation 4.3-1	allowable earthquake load values. 2305.5  16.☐ Hold-down straps - Include the following in design and detailing between floors:
of SDPWS. 2305.3.2  7. ☐ Limit the height-width ratio of the plywood (wood structural panels) shear walls, perforated shear wall segments,	<ul> <li>a. Design and detail straps installation when used as hold-downs across floor joists. Account for reduced number of nails across joist.</li> </ul>
perforated shear walls and shear wall piers to 2:1. Provide complete calculations (including deflection) and details for shear wall with openings.  T' 4.3.4 SDPWS-2008	<ul> <li>Determine the allowable load based on the number of nails through the strap into the posts above and below the "Dead Space" between floors. Specify the number of nails required.</li> </ul>
8. The following applies to all shear walls with a shear values using allowable stress design (ASD) exceed 350 plf or load and resistance factor design (LRFD) exceed 500 plf.  These walls shall be clearly identified on the plans and provided with the following:  2306.3	c. Design and detail straps so that the minimum nail spacing will be provided when the strap nailing is combined with the shear wall edge nailing (i.e. provide 4x member wherever a strap and shear wall edge nailing occur or detail strap nailed over and
<ul> <li>a. 3 x studs and blocks for all framing members receiving edge nailing from abutting panels.</li> </ul>	through un-nailed plywoodshow nailing pattern on plan)
b. 1/2" edge distance from the panel edges and 3/8"	17. Add the following notes on the plans:
from the edge of the connecting members.  c.   All wood structural panel joint and sill plate nailing	<ul> <li>a.  Hold-down connector bolts into wood framing require approved plate washers; and hold-downs shall be finger tight and ½ wrench turn just prior to</li> </ul>
shall be staggered at all panel edges.	covering the wall framing. Connector bolts into wood
<ol> <li>Provide calculations and details for drag struts and drag strut connections to shear walls.</li> </ol>	framing require steel plate washers on the post on the opposite side of the anchorage device. Plate size
10. Provide referenced calculations showing the overturning moments in the shear wall segments.	shall be a minimum of 0.299 inch by 3"x3". <b>2305.5</b>

covering. Face grain of ply	•	P/BC 2014-098 Part C sec B
perpendicular to supports. and groove or blocked pan	el edges. Plywood spans	<ol> <li>Column Weak Axis) (Skewed) (Dual Axis) moment connection is not permitted.</li> </ol>
shall conform to Table 230		P/BC 2014-098 Part C sec B.2
c.  All diaphragm and shear common nails or galvanize		6. ☐ For Reduced Beam Section (RBS) moment connections, comply with AISC 358 Section 5.3 for prequalification
<ul> <li>d. All bolt holes shall be drill oversized.</li> </ul>	ed 1/32" to 1/16" Sec11.1.2.2, 2012 NDS	limits. 7. ☐ For Bolted Unstiffened/Stiffened Extended End Plate
e.  Hold-down hardware mus to foundation inspection.	st be secured in place prior	(BUEEP, BSEEP) moment connections, comply with AISC 358 Section 6.3 for Prequalification limits.  Note: SMF systems in direct contact with concrete
<ul><li>H. <u>STEEL MOMENT FRAME</u></li><li>1. ☐ Structural design drawings and</li></ul>	specifications shall	structural slabs are not prequalified, unless they comply with AISC 358 Section 6.2.
indicate the work to be performe required by AISC 341, AISC Coo Steel Buildings and Bridges, and copy "Standard Quality Assurance	ed, and include items de of Standard Practice for d the 2014 LABC. Obtain a	8. For other prequalified moment connections, comply with AISC 358 Section 7.3, 8.3, 9.3, and 10.3 for prequalification limits.
Frames" sheet 1, 2, and 3; and i plans.		9. Clearly identify on the plan the location and length of the expected plastic hinging zone. No welded, screwed, bolted, or shot-in attachment is permitted within this
<ol><li>Clearly identify in the structural capturents</li><li>plans what type of steel momer</li></ol>		zone. AISC 341 I2-1 and D1-3
building is designed for. Note Resisting System for this build Frame) (Intermediate Moment	on plan "The Lateral Force ding is a (Special Moment	10. Column and beam members used in SMF or IMF shall meet the width-to-thickness ( hd) limitations of T'D1.1 per AISC 341 Chapter D. AISC 341 D1-1b
Moment Frame).		11. Provide a beveled transition detail where changes in
<ul><li>3. ☐ Steel Moment</li><li>a. ☐ Ordinary Moment Frame</li></ul>	IB P/BC 2008-098 is not permitted in Seismic	thickness and width of flanges and webs occur in complete joint penetration groove welded column
Design Category D, E, or F	unless the conditions	splices.  AWS D1.1 2.7.1, 2.16.1.1
below are met. (Refer to Si for Steel Moment Frames f	tructural Design Guidelines for more information.	12. ☐ Column splices shall be located 4 ft or more away
i. ☐ Structural Height of 35 fe	eet	from the beam-to-column flange connections, except:  AISC 341 D2-5a
ii.⊡ Maximum 35 psf dead lo partitions)	ead per floor (including	<ul> <li>a.  When the column clear height between beam-to- column flange connections is less than 8 ft. (2.4 m),</li> </ul>
iii. ☐ Exterior wall weight does	s not exceed 20 psf	splices shall be at half the clear height.
<ul> <li>b.  Intermediate Moment Fra Seismic Design Category E conditions below are met (I Guidelines for Steel Mome information.</li> </ul>	E or F unless the Refer to Structural Design	<ul> <li>b. Column splices with webs and flanges joined by complete-joint-penetration groove welds are permitted to be located closer to the beam-to-column flange connections, but not less than the depth of the column.</li> </ul>
i. ☐ Structural Height of 35 fe	eet	c.  Splices in composite columns.
ii. ☐ Maximum 35 psf dead lo partitions)	ead per floor (including	13. Splice plates or channels used for making web splices in the SFRS columns shall be placed on both sides of the
iii. ☐ Exterior wall weight does	s not exceed 20 psf of wall	column web. Detail this on the plan. AISC 341 D2-5d
<ol> <li>Variations/alterations to prequa connections qualified by cycli haunches or cover plates and deviations/alterations from the</li> </ol>	ic tests, such as additional additional welds, or	14. Groove welds for column splices shall be complete - joint-penetration groove welds that meet the requirement of AISC 341 A3-4b and I2-3 for demand critical welds. Weld tabs shall be re-moved upon completion of weld AISC 341 E3-6a

15. Panel zone doubler plates shall comply with the requirements per AISC 341 E3-6e(3) as:	21. SMF Beams shall be braced to satisfy the require-ments for highly ductile members per AISC 341 D1- 2b  AISC 341 E3-4b
a. Doubler plates in contact with the column web.	
b. Spaced doubler plates.	<ul> <li>a.  Both flanges of beams shall be laterally braced or the beam cross section shall be torsionally braced.</li> </ul>
c. Doubler plates used with continuity plates.	b. The unbraced length between lateral supports shall
d. Doubler plates used without continuity plates.	not exceed $0.086 \text{ r}_y\text{E/F}_y$ . AISC 341 D1-2b
16. Continuity plate for SMF or IMF connections shall be detailed on the plan to match the prequalified connections in AISC 358 or connection prequalified in accordance with Section K1 or tested in accordance with Section K2 of AISC 341. AISC 341 E3-6f	c. Lateral supports shall be provided near concentrated forces, changes in cross-section and other locations where analysis indicates that a plastic hinge will form during inelastic deformations.
<ul> <li>a.  For two-sided connections, the minimum thickness of continuity plate shall be equal to that of the thicker of beam flanges (or beam-flange connection plate). For one-sided connections, continuity plate thickness shall be at least one half of the thickness of the beam flange (or beam-flange connection plate).</li> <li>b.  Continuity plates shall be welded to column webs</li> </ul>	d. ☐ The required strength of lateral bracing shall be M <sub>r</sub> =R <sub>y</sub> F <sub>y</sub> Z (LRFD) or M <sub>r</sub> =R <sub>y</sub> F <sub>y</sub> Z /1.5 (ASD), and the required strength of lateral bracing of each flange provided adjacent to plastic hinges shall be at least; P <sub>u</sub> = 0.06R <sub>y</sub> F <sub>y</sub> Z/h <sub>o</sub> (LRFD) or P <sub>u</sub> = (0.06/1.5)R <sub>y</sub> F <sub>y</sub> Z/h <sub>o</sub> (ASD) and required stiffness shall meet the requirements of Appendix 6 of the AISC 360. AISC 341 D1-2c
using groove welds or fillet welds. AISC 341 E3-6f  17. Continuity plate for OMF connection shall be detailed on the plan in accordance with sections J10.1, J10.2 and	e. The required strength of lateral bracing provided adjacent to plastic hinges for concrete encased composite beams shall be P <sub>u</sub> = 0.06M <sub>p,exp</sub> /h <sub>o</sub> .
J10.3 of AISC 360.  AISC 341 E1–6b  18. SMF When the beam-to-column moment ratio calculated using Equation (E3-1) is more than 2 (column remains elastic), the column flanges shall be laterally supported at the level of the top flanges of the beams.  AISC 341 E3-4c	<ul> <li>22. SMF the individual thicknesses of column webs and doubler plates, shall not be less than that specified in equation (E3-7) per AISC 341 E3-6e (2).</li> <li>23. Column members shall satisfy the requirements of AISC 341 D1-1 for highly ductile members. The compressive axial strength and tensile strength as</li> </ul>
19. SMF When the beam-to-column moment ratio calculated using Equation (E3-1) is less than or equal to 2 (column does not remain elastic), the following requirements shall apply;	determined using the load combinations stipulated in the 2014 LABC including the amplified seismic load  AISC E3-5 and D1-4a
a. Column flanges shall be laterally braced at the levels of both the top and bottom beam flanges. Stability bracing shall be either direct by attaching the lateral bracing element to the column flange at or near the desired bracing point to resist lateral buckling or, alternatively shall be indirect by attached to the column flanges, or rather act through the column web or stiffener plates. AISC 341 E3-4c(1)	<ul> <li>24. The measured flexural resistance of the connection, determined at the column face, shall equal at least 0.80M<sub>p</sub> of the connected beam at an inter-story drift angle of 0.04 (SMF) or 0.02 (IMF) radiansAISC 341 E3-6b</li> <li>25. The required shear strength, V<sub>u</sub>, of the connection shall be based on load combinations per the 2014 LABC that include the amplified seismic load, where the</li> </ul>
b. Each column-flange lateral brace shall be designed for a required strength that is equal to 2 percent of the available beam flange strength Fybftbf (LRFD) or Fybytbf/1.5 (ASD), as appropriate. AISC 341 E3-4c(1)	amplified seismic load due to the effect of horizontal forces is E <sub>mh</sub> = 2(1.1R <sub>y</sub> M <sub>p</sub> )/L <sub>h</sub> . <b>AISC 341 E3-6d</b> 26. ☐ The connection of the frame to the column base shall be designed to transmit forces to the foundation.
20. SMF Where unbraced connections occur in special cases such as two-story frames, atriums and similar architectural spaces. Comply with AISC 341 E3-4c(2) for unbraced Beam-to-Column connections to avoid lateral-torsional buckling of column.  AISC 341 E3-4c(2)	Column base elements include anchor bolts, base plate welds, and any elements that transfer shear, moment, or tension to the foundation.  P/BC 2014-098 Part CsecB.3a

a.  The seismic loads to be transferred to the foundation interface shall be based upon the seismic load combinations.    ASCE 7 sec 12.4.3.2	33. ☐ Provide width-to-thickness ratios of members for OMF to comply with AISC 360 requirements  AISC 341 E1 - 5a
<ul> <li>b. Design of concrete elements at the column base, including anchor rod embedment and reinforcement steel, shall be in accordance with LABC Chapter 19.</li> <li>c. Grade beams shall be provided with ductile detailing per ACI 318 Chapter 21.6 &amp; 21.12.</li> <li>27. Provide calculations to show that the required shear</li> </ul>	<ol> <li>STEEL CANTILEVERED COLUMN</li> <li>Pole Structures shall include the effects of rotation and soil stiffness. Deflection calculations shall be based on approved Soils/Geology Report. Provide a copy of the approved report and the Department's approval letter.         ASCE 7-10 12.13.6.1     </li> </ol>
strength, $R_y$ , of the panel-zone is less than the design shear strength, $R_y$ , of the panel zone.  AISC 341 E3-6e	P-Delta Effect Stress analysis of cantilevered columns shall have an effective length factor of 2.1 for the direction normal to the axis of the beam.  9309.9
28. Members shall be sized to provide strong column/ weak beam in accordance with equation (E3-1) per AISC 341 E3-4a.	3. Special cantilevered columns used as part of the seismic- force resisting system, shall comply with the following:
29. Where column splice occurs, provide calculation to show that the required flexural and shear strength of column splices satisfy AISC 341 E3 - 6g, and AISC 341 D2 -5.	<ul> <li>a.  Maximum axial stress of 15% of allowable.</li> <li>AISC 341-10 sec E5, E6</li> <li>b.  Columns designed as SCCS shall use R, C<sub>d</sub> and factors as per Section G of T' 12.2-1 of ASCE 7-10.</li> </ul>
30. The shape of web access holes shall be in accordance with subclause 6.10.1.2 of AWS D1.8/ D1.8M. Weld access hole quality requirements shall be in accordance with subclause 6.10.2 of AWS D1.8/D1.8M. AISC 341 E1-6b(c)	<ul> <li>c.  The lowest R value shall be used in the same direction unless the building is a Risk Category I or II building that does not exceed 2 stories in height and light frame construction or flexible diaphragms are used.</li> </ul> ASCE 7 sec 12.2.3.3
31. Column and beam members are limited to wide flanges only, except for steel moment frame with "Symmetrical Shapes" in IB P/BC 2014-098 T'1,2,3.	<ul> <li>d.          Columns designed as SCCS shall comply with the requirements of T' D1.1 of AISC 341-10 for highly ductile members.</li> </ul>
32. Fully restrained moment connections that are part of the SFRS shall satisfy at least one of the following requirements:  AISC 341 E-6b	<ul> <li>e.           Columns designed as SCCS shall be braced to satisfy the moderately ductile bracing requirements o         D1.2a of AISC 341-10.</li> </ul>
a.   The required flexural strength shall be equal	i. $\square$ Spacing: $L_b = 0.17r_yE/F_y$
to $1.1R_yM_p$ (LRFD) or $(1.1/1.5)R_yM_p$ (ASD). The required shear strength, $V_u$ or $V_a$ , shall be based on the load combinations stipulated in 2014 LABC	ii. $\square$ Flexural Strength: $M_r = R_y F_y Z$ (LRFD) or $M_r = R_y F_y Z/1.5$ (ASD)
including the amplified seismic load, where the	f.   Label and Dimension Protected Zones
amplified seismic load due to the effect of horizontal forces, including overstrenth is E <sub>mh</sub> = 2 (1.1R <sub>y</sub> M <sub>p</sub> )/L <sub>cf</sub> .  b. ☐ Fully restrained moment connections shall be	<ul> <li>J. PERPENDICULAR TO OPEN WALL LINE</li> <li>1. Maximum allowable shear of Stucco walls with h/b &lt; 2.0 is 100plf.</li> </ul>
designed for a required flexural strength and a required shear strength equal to the maximum moment and corresponding shear that can be transferred to the connection by the system,	Limit the deflection of moment frame to 1.25% for deformation compatibility with (E) stucco wall.
including the effects of material overstrength and strain hardening.	<ul><li>K. <u>FOUNDATION AND GRADING</u></li><li>1. All foundations shall be designed for expansive soil</li></ul>
c. Fully restrained moment connections between wide flange beams and the flanges of wide flange columns shall either satisfy the requirements of section E2.6 or E3.6, or satisfy all conditions listed on	conditions unless a soil report is provided and approved by LADBS Grading Division (see Information Bulletin for more information). Provide details on foundation plans to comply with the requirements.
E1.6b(c)	2. Detail (and reference location on foundation plan) typical foundation sections for: perimeter walls, interior bearing

and garage, garage entrance, spread and/or post pads.	existing footing. Saw cutting the existing footing only
<ul> <li>3. Concrete grade beams that are part of a Moment Frame shall provide transverse reinforcement over a length equal to twice the member depth measured from the face of the supporting member. The spacing of such reinforcement shall not exceed: (a) d/4, (b) 6 times the diameter of the smallest primary flexural rebar excluding longitudinal skin rebar, or (c) 6 inches. The remainder of the grade beam shall have transverse reinforcement spaced not more than d/2.</li> <li>a. ACI 318 Sec 21.3.4.2 and 21.3.4.3 for Intermediate Moment Frames</li> <li>b. ACI 318 Sec 21.5.2, 21.5.3, and 21.5.4 for Special Moment Frames. Grade beams supporting Special Moment frames shall use A706 Reinforcing Steel</li> <li>4. Foundations designed to support cantilevered columns used as part of the SFRS shall have the strength to resist the load combinations with overstrength factor of Section 12.4.3.2 of ASCE 7.</li> <li>5. Provide justification that the proposed cantilever column/grade beam connection detail is fixed as assumed in your design.</li> <li>6. Run frame analysis including grade beam and calculate the deflection of moment frame based on cracked moment of inertia of grade beam.</li> <li>7. Justify grade beam concrete bearing pressure at fixed</li> </ul>	L. FIRE-LIFE SAFETY  1. Fire resistance rated construction. Steel beams an columns shall be protected as required for 1-hour protection. Where ceiling forms the protective membrar for fire-resistive assemblies (occupancy separations an rated roof/ceiling or floor/ceiling assemblies), the construction (floor joists) and their supporting horizonta structural members (beams) need not be individually fir protected except where such members support directly applied loads from more than one floor or roof. The required fire resistance shall not be less than that required rindividual protection of members.  70  2. The means of egress has been compromised due to the strengthening system(s). Provide an alternative path of egress or relocate the strengthening system.  Ch. Provide/dimension the required minimum 7'-0" clear height within the parking area.  406.
base column flange location.	
8. Foundations shall be designed accordingly	
<ul> <li>a.    Bearing capacity shall not exceed the allowable 1806.2</li> </ul>	
b. Resist seismic overturning 1808.3.1	
c. Resist sliding 1605.1.1, 1806.3	
d. Punching shear ACI 318-08, section 11.11.2.1	
9. If fixed end condition is assumed, the concrete grade beam shall be designed as a moment reaction.	
<ul><li>10. Foundations with stem walls shall be reinforced with a minimum of two No. 4 bars at the top of the wall and two No. 4 bars at the bottom of the footing.</li><li>1908.1.8</li></ul>	
<ul><li>11. Site drainage: Show on plans how concentrated drainage is being conveyed to the street via non-erosive devices.</li><li>7013.10</li></ul>	
12. Add note on the plans:	
<ul> <li>a.  If adverse soil conditions are encountered, a soils investigation report may be required. 1803.5.2</li> </ul>	

ADDITIONAL COMMENTS		
Items	Code Sec.	